# APPENDIX C HYDROLOGY REPORT



# **Existing On-Site Storm Drain Analysis**

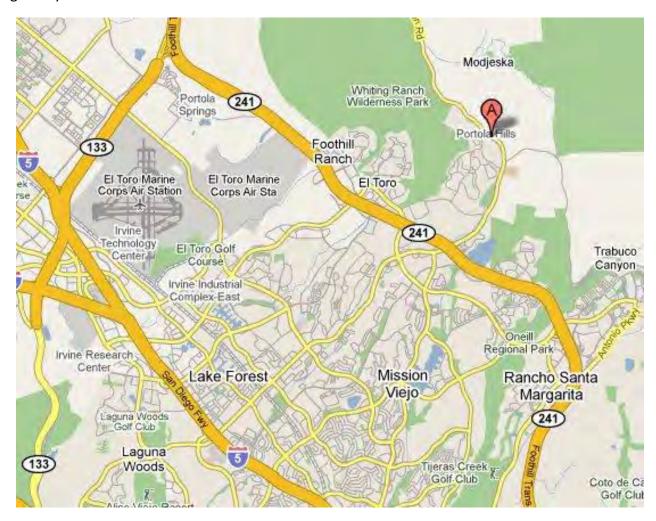
# Rancho Las Lomas 19191 Lawrence Canyon Orange County, California 92667

#### **Prepared By:**

Trithis Engineering 1524 Brookhollow Dr. – Suite C Santa Ana, CA 92705 949-642-7442

#### Introduction:

The project, Rancho las Lomas (RLL), consisting of approximately 20 acres is located directly west of and adjacent to Santiago Canyon road about 1000 feet northerly of the junction of Santiago Canyon Road and Live Oak Canyon Road in Orange County, California. It is traversed from north to south by Santiago Canyon Road and by Alisos Creek, which meanders through the project as a natural drainage course in which several culverts and bridges have been constructed for road crossings. Also, an earth levee approximately 10 feet high and 750 feet long has been constructed between the east side of the natural drainage course and Santiago Canyon Road.



# **VICINITY MAP (SITE 'A')**

The drainage area consists of 678.5 acres and varies from elevation 2200 at the north end and to elevation 1111 at the south end as shown on the El Toro and Santiago Peak U.S.G.S. Quadrangle Maps. At present, the drainage area has undergone residential development to the east modifying its natural state, which consisted of chaparral, open brush, and some live oak trees. This new development has modified the flow characteristics to 2 drainage structures crossing Santiago Canyon Road from the east and discharging into Alisos Creek, which flows north to south through RLL.

The purpose and intent of this report is to analyze the existing onsite drainage collection system to provide operational characteristics in 10 and 100 year storm events. All onsite drainage flows directly to Alisos Creek either by sheet/surface flow or by the onsite storm drain collection system which then discharges into Alisos Creek through drain line which daylights onto rip rap energy dissipaters roughly 10'x10' in area, minimum 6" Class 2 Rock with no grout.



**SITE AERIAL PHOTO** 

We have analyzed each drainage collection zone for Q10 and Q100 storm events. Rainfall data has been obtained the Orange County Hydrology Manual Figure B-4 Mean Precipitation Intensities for Mountainous Area which follows. We have elected to use the simplified rational method to calculate the storm flows from each watershed as directed by the Orange County Hydrology Manual. We have submitted hydrology reports for this project in the past and that has proven to be an acceptable method of analysis for this existing project's storm collection and conveyance system.

### **Design Engineering:**

The volume of runoff has been estimated using the formula known as the Rational Method (Q=ACI) where 'Q' = flow in CFS, 'A' = area drained in acres, 'C' = coefficient of runoff and 'I' = intensity of rainfall in inches per hour. The intensity (I) of rainfall used for these calculations is 1.25"/hr (10 year storm event) and 1.95"/hr (100 year storm event).

We have elected to use the Rational Method in its most basic form without including calculation for time of concentration (Tc), nor any adjustments due to infiltration. We have also used runoff coefficients which we consider very conservative and not incorporated "Area Averaged" calculations to raise or lower the coefficients to more liberal flow reductions. The calculations have been performed with the assumption that all systems are running at maximum flow for the given storm event.

The calculation sheet (PAGE 5) lists each drainage pipe installed at the site in the first column. Please use the included scale drawing of the site for Line and Area Reference. In addition the chart address's the following information:

- 1. Drainage area Runoff Coefficient
- 2. Rainfall for R Q10 10 year storm event
- 3. Rainfall for R Q100 100 year storm event
- 4. Drainage area collected in Acres
- 5. Flow for 10 year event (F Q10) in Cubic Feet per Second.
- 6. Flow for 100 year event (F Q100) in Cubic Feet per Second.
- 7. Slope of collector pipe in percent grade.
- 8. Type of pipe installed, PVC, RCP or CMP
- 9. Roughness Coefficient 'n' for installed pipe.
- 10. Size of pipe that would have been specified had this project be in the preliminary design phase of development.
- 11. Size of pipe as it is installed at the project site.
- 12. Maximum flow that the installed pipe will convey as it is currently installed at the project site.

#### ORANGE COUNTY PRECIPITATION DATA (inches)

#### DURATION 6H T-YR. 5M 30M 1H 3H 24H 100 0.52(.78) 1.09(1.34) 1.45(1.94) 2.43(3.96) 3.36(6.19) 5.63(11.27) 50 0.45(.71) 0.98(1.19) 1.30(1.73) 2.19(3.52) 3.02(5.51) 5.07(10.02) 25 0.40(.63) 0.87(1.04) 1.15(1.51) 1.94(3.08) 2.71(4.81) 4.49(8.76) 10 0.34(.50) 0.72(.84) 0.95(1.22) 1.59(2.48) 2.20(3.87) 3.68(7.05) 5 0.26(.40) 0.59(.68) 0.78(.99) 1.31(2.01) 1.81(3.14) 3.03(5.71) 2 0.19(.26) 0.40(.45) 0.53(.66) 0.89(1.34) 1.22(2.09) 2.05(3.81) NOTES:

- (1.) Numbers in ( ) are from the Santiago Peak gage station #156 Use in areas above 2,000 feet in elevation.
- (2.) Precipitation data for nonmountainous areas taken from an average of 25 rain gages. Use in areas below 2,000 feet in elevation.
- (3.) All 5M values are extrapolations
- (4.) M = minutes; H = hours.

Rancho Las Lomas On-Site Drainage System Analysis

Pipe #	Runoff 'C'	R Q10	R Q100	Acres	F Q10	F Q100	Slope %	Pipe	Roughness 'n'	Design Size	Installed Size	Max Flow CFS
L1	0.95	1.25	1.95	0.99	1.18	1.83	13	PVC	0.009	6"	12"	23.00
L2	0.95	1.25	1.95	1.95	2.32	3.61	6	CMP	0.022	10"	12"	5.50
L3	0.95	1.25	1.95	0.79	0.94	1.46	20	RCP	0.012	6"	12"	17.00
L4	0.95	1.25	1.95	0.97	1.15	1.80	2	RCP	0.012	8"	12"	5.50
L5	0.20	1.25	1.95	4.57	1.14	1.78	2	RCP	0.012	8"	12"	6.00
L6	0.95	1.25	1.95	1.35	1.60	2.50	2	CMP	0.022	10"	12"	3.25
L7	C1	1.25	1.95	6.81	3.90	6.08	23	CMP	0.022	10"	18"	25.00
L8	0.95	1.25	1.95	1.22	1.45	2.26	21	PVC	0.009	6"	12"	20.00
L9	0.95	1.25	1.95	0.72	0.86	1.33	2	PVC	0.009	6"	6"	1.30
L10	0.95	1.25	1.95	0.42	0.50	0.78	42	PVC	0.009	4"	6"	4.00
L11	0.20	1.25	1.95	2.09	0.52	0.82	28	CMP	0.022	4"	12"	11.00
L12	0.95	1.25	1.95	3.41	4.05	6.32	21	CMP	0.022	10"	12"	6.00
L13	0.20	1.25	1.95	1.53	0.38	0.60	22	PVC	0.009	4"	12"	22.00
L14	0.95	1.25	1.95	0.16	0.19	0.30	2	PVC	0.009	4"	6"	1.30
L15	0.95	1.25	1.95	0.14	0.17	0.26	9	PVC	0.009	4"	6"	2.80
L16	0.35	1.25	1.95	0.32	0.14	0.22	6	RCP	0.012	4"	18"	31.00
L17	0.95	1.25	1.95	0.09	0.11	0.17	1	PVC	0.009	4"	4"	1.30
L18	0.95	1.25	1.95	0.28	0.33	0.52	6	RCP	0.012	4"	18"	22.50
L19	0.95	1.25	1.95	0.09	0.11	0.17	36	PVC	0.009	4"	6"	5.00
L20	0.95	1.25	1.95	0.20	0.24	0.37	36	PVC	0.009	4"	6"	5.00
L21	0.95	1.25	1.95	0.19	0.23	0.35	2	PVC	0.009	4"	6"	1.41
L22	0.95	1.25	1.95	0.19	0.23	0.35	2	PVC	0.009	4"	6"	1.41
L23	0.95	1.25	1.95	0.20	0.06	0.37	40	PVC	0.009	4"	4"	1.70
L24	0.95	1.25	1.95	0.14	0.17	0.26	15	PVC	0.009	4"	4"	1.20
L25	0.95	1.25	1.95	0.28	0.33	0.52	35	PVC	0.009	4"	4"	1.70
L26	C2	1.25	1.95	0.20	0.24	0.37	37	PVC	0.009	4"	8"	1.85
L27	0.95	1.25	1.95	0.17	0.20	0.31	43	PVC	0.009	4"	6"	1.80
L28	C3	1.25	1.95	1.33	1.58	2.46	43	PVC	0.009	4"	8"	7.75
L29	0.95	1.25	1.95	1.28	0.06	2.37	19	PVC	0.009	4"	12"	22.00
L30	0.95	1.25	1.95	0.82	0.97	1.52	37	PVC	0.009	4"	12"	26.00
L31	0.95	1.25	1.95	0.08	0.10	0.15	27	PVC	0.009	4"	6"	3.20

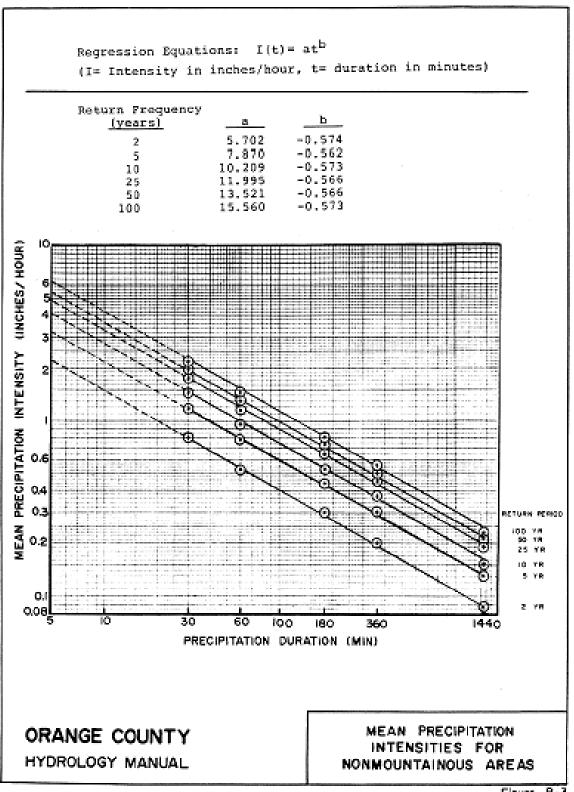
C1	Collector Pipe from L4, L5 and L6
C2	Collector Pipe from L15 and L24
C3	Collector Pipe from L21

#### **Summary:**

It is noted that given the various rainfall intensity data available from Orange County and the historical data available from NOAA Western U.S. Precipitation Frequency Maps it is hard to decide which data to use. The chart above was developed using Orange County Mean Precipitation for Mountainous Areas when we discovered we can use Figure B3 on page 6 or "Nonmoutainous" area less than elevation 2000. This chart significantly reduces the historical rainfall we chose to use and allows us to look at time of concentration of less than 60 minutes. Give the data listed in Figure B3 and reviewing our Q10 flow rates listed above we feel that the pipe listed would still perform at double the flows listed which eliminates the need to recalculate the chart which would prove nothing more.

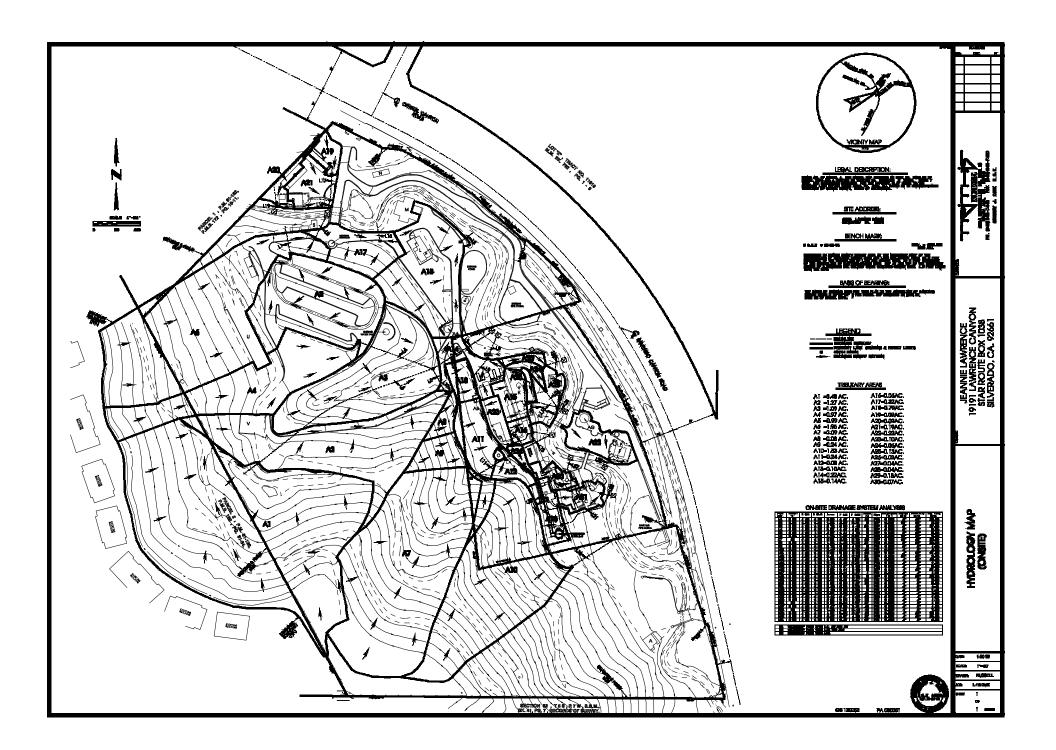
After reviewing all drain lines within the site it is determined that all meet and exceed standard engineering practices for drain line engineering. All lines will convey both Q10 and Q100 storm events. In the event of a

blockage to a drainage inlet over land release will follow the natural and manmade drainage courses ultimately ending up in Aliso Creek confined within the property limits.



B~7

Figure B-3



# **Site Plan & Drainage System Engineering Exhibits:**

1. See Hydrology Map (ONSITE) attached 50 scale map for drain line and drainage area delineation. Scale 1''=50'.

**End of Report** 

# A Flood Plain Calculations

19191 Lawrence Canyon
Orange County, California 92667



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## May 27, 2002Introduction

The project, Rancho las Lomas (RLL), consisting of approximately 20 acres is located directly west of and adjacent to Santiago Canyon road about 1000 feet northerly of the junction of Santiago Canyon Road and Live Oak Canyon Road in Orange County, California. It is traversed from north to south by Santiago Canyon Road and by Alisos Creek, which meanders through the project as a natural drainage course in which several culverts and bridges have been constructed for road crossings.

The drainage area consists of 678.5 acres and varies from elevation 2200 at the north end and to elevation 1111 at the south end as shown on the El Toro and Santiago Peak U.S.G.S.

Quadrangle Maps used in the report update (see Drainage Area Map 'A' & Drainage Area Concentration Point Map 'B' on page 4). At present, the drainage area has undergone residential development to the east modifying its natural state, which consisted of chaparral, open brush, and some live oak trees. This new development has modified the flow characteristics to 2 drainage structures crossing Santiago Canyon Road from the east and discharging into Alisos Creek, which flows north to south through RLL.

The purpose and intent of this report is to further analyze the data from the Carlat report and present the results due to modifications and improvements to the Alisos Creek section running through the RLL site. The flow database used in this report was calculated and updated over a 10 year period by Carlat Engineering and is considered current and a part of this report. The modifications presented herein were to provide control and containment that is more positive in a Q<sub>100</sub> storm event. We have developed a database for computer analysis of the entire flow line of Alisos Creek through the project. The 100-year flood limits as discovered in the Carlat Report are indicated on insert Exhibit A. Present modifications result in the 100-year flood plain being contained within the limits of the creek bed (see attached "Exhibit - A").

The data and changes presented in this report were developed based on the previous as-built data for the property. Flow through the site encountered numerous structural modifications which reduce and accelerate velocities in feet per second (fps) causing numerous hydraulic jumps and headwater backup. The system could not keep itself clean and provided numerous locations for silt and debris trapping which further raised the flood water level over time. The computer models cross section utilized 1:1 side banks with a flat bottom for the main creek flow line. Modified concrete culverts similar to the sketch section that follows are used for all the crossings except the pedestrian bridge to the restrooms. Grades at various nodes have been modified to return the creek bed to it's original gradient to allow for more consistent and balanced flow in fps thus eliminating numerous hydraulic jumps which occurred at locations of high flow rates converging with relatively flat & slow sections. The computer model section was developed to offer a basis for study of velocities and area required to maintain a fixed volume of water through these sections at a fixed velocity. The creeks cross sections have been modified with more relaxed side slopes as conditions allow along the flow line. This has a negligible effect on the coefficient of friction within the sections length. It is the volume of water and the velocities that it is traveling that are the constants and have been be adhered to in the final engineering documents for the proposed one hundred year flood limits to be achieved.

#### Reference Materials

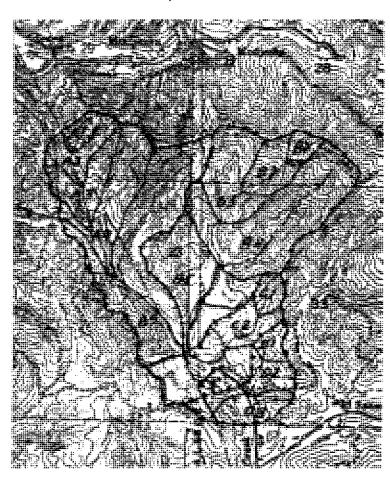
Hydrology/Hydrodynamic Assumptions & Criteria are based on the following reference materials:

- 1) "Orange County Hydrology Manual" Dated March 12, 1991.
- 2) Orange County E.M.A. "Drainage Design Criteria Aids" dated February 1982.
- 3) "Hydrology and Flood Plain Calculations for 19191 Lawrence Canyon Orange County, California 92667" prepared by Carlat Engineering 3812 E. La Palma Avenue Anaheim, CA 92807 dated November 15, 1989 and revised November 30, 1992. The following data/tables are included in this report for clarity and historical reference only:
  - a) Hydrology Criteria
  - b) Calculation of Area-weighted Pervious Area Fraction
  - c) Watershed Information Form (Figure E-5).
  - d) Area Averaged Mass Rainfall Plotting Sheet for entire watershed 100-year 24 hour storm adjusted by area weighting for mountainous portion and for depth area. (Figure B-

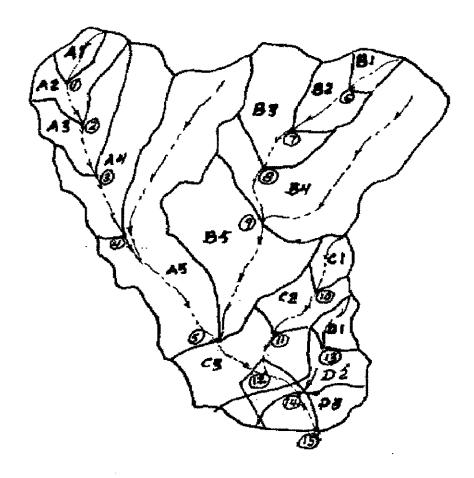
- e) Mean Precipitation Depths for Non-Mountainous Areas (Figure B-1)
- f) Mean Precipitation Depths for Mountainous Area (Figure B-2)
- g) Mean Precipitation Intensities for Non-Mountainous Areas (Figure B-3)
- h) Mean Precipitation Intensities for Mountainous Areas (Figure B-4)
- i) Time of Concentration Nomograph for Initial Subarea (figure D-1).
- j) Velocity Discharge Slope Relationships, Natural Valley Channels (Plate D-6.1).
- k) Slope Adjustment Curve for Natural Mountain Channel (Plate D-6.2).
- 1) Velocity Discharge Slope Relationships, Natural Mountain Channels (Plate D-6.3)
- m) Rational Study Method Form (Figure D-4) 100-year storm rational method study.
- 4) Water Surface Profile Listing
- 5) Hydrology & Flood Plain Delineation Exhibit A 100-year Flood Containment Plan.

### **Observations, Conclusions and Recommendations**

Please reference "Hydrology - Exhibit A - Q100 Flood Limits" (attached). All cross sectional dimensions are indicated on the following "Water Surface Profile Listing" (Note: depths listed in the calculations are hypothetical. Water surface elevations are critical):



DRAINAGE AREA MAP 'A'



## DRAINAGE AREA CONCENTRATION POINT MAP 'B'

May 6, 2002 9:26:14

#### WATER SURFACE PROFILE LISTING Rancho Las Lomas - Q100 flood Plain Analysis Created: May 2002 Greg Cook RCE - Dave Snead Hydrologist

0 STATION ZL NO AV	INVERT	DEPTH	W.S.	Õ	VEL	AET	ENERGY	SUPER	CRITICAL		HGT/	BASE/
PIER	ELEV	OF FLOW	ELEV			HEAD	GRD.EL.	ELEV	DEPTH		DIA	ID NO.
0 L/ELEM 2R	so					SF AVE	HF		ИО	RM DEPTH		
******	*****	****	*****	****	*****	*****	*****	****	*****	*****	****	*****
******							7					
Node 1 -SYS												
	1111.80 0.00	6.62	1118.42	1752.0	15.29	3.63	1122.05	0.00	7.19		7.00	14.00
	1111.80 0.00	6.62	1118.42	1752.0	15.29	3.63	1122.05	0.00	7.19		7.00	14.00
	0.03440					0.03388	0.37			6.60		
	1112.17	6.64	1118.81	1752.0	15.24	3.61	1122.42	0.00	7.19		7.00	14.00
	0.03440					0.03165	0.67			6.60		
0 32.03	1112.90	6.91	1119.81	1752.0	14.53	3.28	1123.09	0.00	7.19		7.00	14.00
	0.03440					0.02776	0.08			6.60		

Node 2 OTRANS STR 0.00000					0.02594	0 00					
0.50 0 34.88 1113.00	7 19	1120 10					n 92	7 10		7 00	14 00
0.50 0 0.00 0 5.89 0.02420		1120.15				0.15			7.34		14.00
0_50		* <b>* * * *</b> * * * * * * * * * * * * * *									
( 40.77 1113.14 0 0.00		1120.48									14.00
0 35.43 0.02420 0.50						0.86					
0 76.20 1114.00 0.50 0 0.00	7.34	1121.34	1752.0	13.51	2.84	1124.18	0.00	7.19		7.00	14.00
Node 3 OTRANS STR 0.00000					0.01547	0.00					
0.50 0 76.20 1114.00	9.27	1123,27	1752.0	8.35	1,08	1124.35	1.76	6.26		6.00	18.00
0.50 0 0.00 0 12.69 0.02704						0.09					
0.50 0 88.89 1114.34		1123.25	. 1752.0								18.00
0.50 0 0.00 0 12.15 0.02704		1,,40,130	110010			0.10			6.05		10.00
0.50 0 101.04 1114.67		1100 00	1750 0								30.00
0.50 0 0.00		1123.23	1732,0						6.05		18.00
0 11.59 0.02704 0.50		1102 21	1750 0			0.11			6.05		40.00
0 112.64 1114.99 0.50 0 0.00		1123.21									18.00
0 11.02 0.02704 0.50						0.12					
0 123.65 1115.28 0.50 0 0.00	7.90	1123.18									18.00
0 10.41 0.02704 0.50						0.13					
0 134.06 1115.56 0.50 0 0.00	7.58	1123.15	1752.0	10.60	1.75	1124.90	2.66	6.26		6.00	18.00
0 9.73 0.02704 0.50						0.14			6.05		
0 143.79 1115.83 0.50 0 0.00	7.28	1123.11	1752.0	11.12	1.92	1125.03	2.89	6.26		6.00	18.00
6.37 0.02704					0.01556	0.10			6.05		
0 150.16 1116.00 0.50 0 0.00	7.08	1123.08	1752.0	11.50	2,05	1125.13	0.00	6.26		6.00	18.00
Node 4 OTRANS STR 0.00000					0.01398	0.00					
0.50 0 150.16 1116.00	7.57	1123.57	1752.0	10.15	1.60	1125.17	0.00	6.07		6.00	19.00
0.50 0 0.00 0 3.10 0.05147					0.01235	0.04			4.79		
0.50 0 153.26 1116.16	7.32	1123.48	1752.0	10.56	1.73	1125.21	0.00	6.07		6.00	19.00
0.50 0 0.00 OHYDRAULIC JUMP											
0.50 0 153.26 1116.16	4.96	1121.12	1752.0	16.45	4.21	1125.32	0.00	6,07		6.00	19.00
0.50 0 0.00 0 19.55 0.05147						0.85			4.79		
0.50 0 172.81 1117.17		1122.32	1752.0	15.75	3.85	1126.18	0.00				19.00
0.50 0 0.00 0 9.39 0.05147						0.36			4.79		
0.50 0 182.20 1117.65	5.38	1123.03						6.07			19 00
0.50 0 0.00 0 4.69 0.05147		***				0.16		0.07			13.00
0.50 0 186.89 1117.89		1100 50									10.00
0.50 0 0.00 0 2.13 0.05147		1140.00	1102.0			0.06					19.00
0.50		2100 00	1750 0					<i>(</i> 07			10.00
0 189.02 1118.00 0.50 0 0.00	3.65	1143.62	1/32.0	13.05	2.90	1120.75	U.UU	6.07		b.U0	TA'00
Node 5 OTRANS STR 0.00000					0.03354	0.00					
0 50 189.02 1118.00	5.47	1123.47	1752.0	14.74	3.38	1126.85	1.11	6.07		6.50	19.00
( ,J 0 0.00 0 1.19 0.02041					0.03394	0.04			6.38		
0.50 0 190.21 1118.02	5.43	1123.45									19.00
0.50 0 0.00 0 7.15 0.02041						0.26					
0.50											

					•						
0 -197.36 1118 0.50 0 0.00	5.20	1123.37	1752.0	15.59	3.78	1127.15	1.23			6.50	19.00
0 7.34 0.02 0.50	041				0.04229	0.31			6.38		
0 204.70 1118 0.50 0 0.00 Node 6 Bridge Ou		1123.31	1752.0	16.35	4.15	1127.46	0.00	6.07		6,50	19.00
NS STR 0.00					0.04149	0.00					
0 204.70 1118	5.46	1123.78	1752.0	15.48	3.72	1127.50	0.00	6.26		7.50	18.00
0.50 0 0.00 0 5.92 0.01	.691				0.01145	0.07			4.86		
0.50 0 210.62 1118	1.42 5.52	1123.94	1752.0	15.28	3.63	1127.57	0.00	6.26		7.50	18.00
0.50 0 0.00 0 14.62 0.01	.691				0.01052	0.15			4.86		
0.50 0 225.24 1118	5.76	1124.43	1752.0	14.57	3.30	1127.73	0.00	6.26		7.50	18.00
0.50 0 0.00 0 7.03 0.01	.691				0.00919	0.06			4.86		
0.50 0 232.28 1118	6.00	1124.79	1752.0	13.89	3,00	1127.79	0.00	6.26		7.50	18.00
0.50 0 0.00 0 1.99 0.01	.691				0.00803	0.02			4.86		
0.50 0 234.27 1118		1125.08	1752.0	13.25	2.73	1127.81	0,00	6.26		7.50	18.00
		•									
OTRANS STR 0.00					0.01953	0.00					
0 234.27 1118 0.50 0 0.00	.82 7.16	1125.98	1752.0	11.08	1.91	1127.89	0.00	6.16		8.00	18.50
0 43.51 0.01	.333				0.01442	0.63			7.39		
0.50 0 277.78 1119	7.28	1126.68	1752.0	10.87	1.84	1128.52	0.00	6.16		8.00	18.50
0.50 0 0.00 Node 8 OTRANS STR 0.00	000				0.01305	0.00					
0.50 0 277.78 1119	.40 7.49	1126.89	1752.0	10.28	1.64	1128.54	3.75	6.07		8.00	19.00
0.50 0 0.00 0 8.88 0.02	837				0.01294	0.11			5.76		
0 50 286.66 1119	.65 7.19	1126.84	1752.0	10.78	1,81	1128.65	4.08	6.07		8.00	19.00
0 0.00 0 8.09 0.02						0.12			5.76		
0.50 0 294.74 1119		1126.78	1752.0	11.31	1 - 99	1128.77	4.44	6.07			19.00
0.50 0 0.00 0 4.19 0.02					0.01640				5.76	**	
0.50 0 298.93 1120		1126.74	1752.0	11.62	2.10	1128.84	0.00	6.07		8.00	19.00
0.50 0 0.00 Node 9										_,	
OTRANS STR 0.00 0.50						0.00					
0 298.93 1120 0.50 0 0.00	.00 8.42	1128.42	1752.0	6.09	0.58	1128.99	0.10	4.61	·	8.00	30.00
0 6.07 0.05 0.50											
0 305.00 1120 0.50 0 0.00	.31 8.07	1128.38	1752.0	6.38	0.63	1129.01	0.11	4.61		8.00	30.00
0 5.73 0.05 0.50	168				0.00393	0.02			3.55		
0 310.73 1120 0.50 0 0.00	.61 7.73	1128.34	1752.0	6,69	0.70	1129.03	0.12	4.61		8.00	30.00
0 5.40 0.05 0.50	168				0.00451	0.02			3.55		
0 316.13 1120 0.50 0 0.00	.89 7.40	1128.29	1752.0	7.02	0.77	1129.06	0.14	4.61		8.00	30.00
0 2.15 0.05	168				0.00496	0.01			3.55		
0.50	.00 7.27	1128.27	1752.0	7.16	0.80	1129.07	0.14	4.61		8.00	30.00
0.50 0 0.00 0 0.00 0.05	168				0.00511	0.00			3.55		
0.50 0 318.28 1121		1128.27	1752.0	7.16	0.80	1129.07	0.00	4.61		8.00	30.00
0.50 0 0.00 10 - 48" CM CT STR 0.00	P from off-si	lte			0.00487	0.00					
0.50 0 318.28 1121	.00 7.37	1128.37	1708.0	6.88	0.73	1129.11	1.96	4.53		8.00	30.00
0.50 0 0.00 0 11.50 0.02	561				0.00499	0.06			4.34	F _	
0.50 0 329.78 1121		1128.36									30.00

0.50 0												
0 10.96 0.50												
0 340.73 0.50 0	1121.57 0.00	6.76	1128.34	1708.0	7.56	0.89	1129.23	2.33	4.53		8.00	30.00
	0.02561					0.00639	0.04			4.34		
347.02	1121.74	6.59	1128.33	1708.0	7.78	0.94	1129.27	2.45	4.53		8.00	30.00
OHYDRAULIC 0.50												
	1121.74	2.94	1124.68	1708.0	18.45	5.29	1129.97	12.42	4.53		8.00	30.00
0 5.07						0.09695	0.49			4.34		
	1121.87	2.82	1124.69	1708.0	19.26	5.76	1130.45	13.48	4.53		8.00	30.00
	0.00 0.02561					0.11170	0.58			4.34		
0.50 0 357.33	-1122.00	2.70	1124.70	1708.0	20.20	6.34	1131.04	0.00	4.53		8.00	30.00
0.50 0 Node 11	0.00			•								
OTRANS STR 0.50						0.07249						
0 357.33 0.50 0	1122.00 0.00	6.58	1128.58	1708.0	13.45	2.81	1131.39	1.66	6.58		8.00	16.00
	0.01364					0.02344	0.04			7.92		
0 359.11 0.50 0	1122.02	6.86	1128.88	1708.0	12.82	2.55	1131.44	1.53	6.58		8.00	16.00
0 7.33 0.50						0.02053	0.15			7.92		
0 366.44	1122.12	7.14	1129.26	1708.0	12.22	2.32	1131.59	1.40	6.58		8.00	16.00
0.50 0 0 18.80						0.01799	0.34			7.92		
	1122,38	7,43	1129.81	1708.0	11.66	2.11	1131.92	1.29	6.58		8.00	16.00
	0.00 0.01364					0.01642	0.22			7.92		
	1122.56	7.54	1130.10	1708.0	11.46	2.04	1132.14	0.00	6.58		8.00	16.00
0.50 0 V 12												
0.50	0.00000					0.01603						
0 398.38 0.50 0	1122.56 0.00	7.54	1130.10	1708.0	11.46	2.04	1132.14	0.30	6.58		8.00	16.00
0 97.77 0.50	0.01473					0.01543	1.51			7.74		
	1124.00	7.72	1131,72	1708.0	11.14	1.93	1133.65	0.00	6,58		8.00	16.00
Node 13 OTRANS STR						0.00929	0 00					
0.50	1124.00	0.10	1122 30	3700 A	6 67			0 66	F 20		9 00	24 00
0.50 0	0.00		1133.10	1700.0	0.57		0.06					24.00
0.50	0.02498		****	1500 0	5 00							0.1.00
0.50 0			1133.09	1708.0								24.00
0.50	0.02498						0.06					
0 524.23 0.50 0	1124.70 0.00	8.38	1133.08	1708.0					5.20			24.00
0.50	0.02498						0.07			5.06		
0 537.43 0.50 0	1125.03 0.00	8.04	1133.07	1708.0	7.58	0.89	1133.97	0.85	5.20		8.00	24.00
	0.02498					0.00601	0.08			5.06		
	1125.35	7.71	1133.06	1708.0	7.95	0.98	1134.04	0.92	5.20		8.00	24.00
	0.02498					0.00689	0.08			5.06		
0 562.15	1125.65	7.40	1133.04	1708.0	8.34	1.08	1134.12	1.00	5.20		8.00	24.00
	0.00498					0.00766	0.05			5.06		
0.50	1125.82	7.21	1133.03	1708.0	8.58	1.14	1134.18	0.00	5.20		8.00	24.00
0J 0 Node 14												
OTRANS STR 0.50							0.00					
0.50 0		7.21	1133.03	1708.0	8.58	1.14	1134.18	1.41			8.00	24.00
0 42.29						0.00803	0.34			7.07		

0.50											
0.50 0 611.30 1126.18 0.50 0 0.00	7.18	1133.36	1708.0	8.62	1.15	1134.52	0.00	5.20		8.00	24.00
Node 15 OTRANS STR 0.00000											
0.50 0611.30 1126.18	5.74	1131.92	1708.0	14.25	3.16	1135.08	0.00	6.16		8.00	18.00
0 0.00 N = 16 Pedestrian Br	idge Outl	iet									
0TRANS STR 0.00000 0.50					0.04793						
0 674.03 1128.00 0.50 0 0.00								6.58		7.00	16.00
0 674.03 1128.00 0.50 0 0.00	5.68	1133.68	1708.0					6.58		7.00	16.00
0 1.60 0.06136 0.50						0.02			3.47		
0 675.63 1128.10 0.50 0 0.00		1133.92	1708.0					6.58		7.00	16.00
0 1.88 0.06136 0.50			· ·		0.01080	0.02			3.47		
0 677.52 1128.21 0.50 0 0.00	6.07	1134.28	1708.0				0.00	6.58		7.00	16.00
0 1.07 0.06136 0.50					0.00944	0.01			3.47		
0 678.58 1128.28 0.50 0 0.00	6.32	1134.60	1708.0	14.11	3.09	1137.69	0.00	6.58		7.00	16.00
0 0.34 0.06136 0.50					0.00826	0.00			3.47		
Node 17 Pedestrian Br OTRANS STR 0.00000	idge Inle	et			0.02499	n nn					
0.50 0 678.92 1128.30	<i>C</i>	1124 88	1709 0				0.23	6 58		7 00	16.00
0.50 0 0.00	0.30	1134.00	1,00.0			0.09			6.68		10.00
0 3.88 0.02386 0.50	5 50	1105.03	1700 0								16.00
0 682.80 1128.39 0.50 0 0.00	6.68	1135.07	1/08.0								16.00
0 67.37 0.02386 0.50						1.61					
0 750.17 1130.00 0.50 0 0.00	6.68	1136.68	1708.0	13.23	2.72	1139.40	0.00	6.58		7.00	16.00
18 NS STR 0.00000			•		0.02273	0.00					
0.50 0 750.17 1130.00 0.50 0 0.00	6.88	1136.89	1708.0	12.76	2.53	1139.42	2.82	6.58		7.00	16.00
0.50 0 0.00 0 6.71 0.02019 0.50					0.02143	0.14			7.03		
0 756.88 1130.14	6.92	1137.05	1708.0	12.69	2.50	1139.56	2.79	6.58		7.00	16.00
0.50 0 0.00 OHYDRAULIC JUMP											
0.50 0 756.88 1130.14	6.25	1136.39	1708.0	14.28	3.17	1139.56	3.43	6.58		7.00	16.00
0.50 0 0.00 0 1.36 0.02019					0.02999	0.04			7.03		
0.50 0 758.24 1130.16	6.20	1136.36	1708.0	14.43	3.24	1139.60	3.50	6.58		7.00	16.00
0.50 0 0.00 0 5.96 0.02019					0.03261	0.19			7.03		
0.50 0 764.20 1130.28	5.95	1136.23	1708.0	15.13	3.56	1139.79	3.80	6.58		7.00	16.00
0.50 0 0.00 0 6.75 0.02019					0.03729	0.25			7.03		
0.50 0 770.95 1130.42	5.71	1136.13	1708.0	15.87	3.92	1140.04	4.14	6,58		7.00	16.00
0.50 0 0.00 0 7.11 0.02019					0.04265	0.30			7.03		
0.50 0 778.05 1130.56	5.48	1136.04	1708.0	16.65	4.31	1140.35	4.50	6.58		7.00	16.00
0.50 0 0.00 0 7.24 0.02019						0.35					
0.50 0 785.29 1130.71		1135.96							7,00		16.00
0.50 0 0.00 0 7.24 0.02019						0.40		0.30			_ 3 . 3 .
0.50 0 792.54 1130.86		1135 99									16 AA
0 0.00 0 7.16 0.02019		2200.03	1,00.0			0.46			7.03		70.00
0.50 0 799.70 1131.00		1134 63	17กล ก								16.00
							0.00	0,00		7. UV	20.00
0.50 0 0.00 Node 19 Pedestrian Bi OTRANS STR 0.00000	rade Ont	16.			0.05052	0.00					
0.50											

0.50 0		6.25	1137.25	1708.0					7.66		7.00	12.00
0 5.50 0.50							0.17			7.07		
0.50 0			1137.57	1708.0							7.00	12.00
9-1	0.03555						0.09			7.07		
0.50 0	1131.30 0.00	6.66	1137.96	1708.0	14.08	3.08	1142.04	0.00	7.66		7.00	12.00
Node 20 Pe OTRANS STR	destrian Bri 0.00000	ldge Inl	et			0.01850	0.00					
0.50 0 808.14	1131.30	7.47	1138.77	1708.0	9.63	1,44	1142.21	0.00	7.08		7.00	14.00
0.50 G							0.24			7.67		
0.50	1131.75	7.11	1138.86	1708.0							7 00	14 00
0.50 0							0.15			7.67	7.00	14.00
0.50	1132.00	רם ד	1320 02	1709 A					7.08		7 00	14 00
0.50 0	0.00	1.92	1130.92	1708.0	10.37	1.0/	1142.59	0.00	7.08		7.00	14.00
OHYDRAULIC 0.50	OOMP											
Node 21 OTRANS STR	0.00000					0.01201	0.00					
	1132.00	5,89	1138.23	1708.0	17.13	4.56	1142.79	1.78	7.08		8.00	14.00
0.50 0 0 25.94						0.04573	1.19			5,78		
	1133.65	6.03	1139.68	1708.0	16.66	4.31	1143.99	1.69	7.08		8.00	14.00
0,50 0 0 15.89	0.00 0.05027					0.04123	0.65			5.78		
0.50 0 892.17	1134.45	6.28	1140.73	1708.0	15.88	3.92	1144.65	1.56	7.08		8.00	14.00
0.50 0 0 7.01	0.00					0.03613	0.25			5.78		
0.50		6.53	1141.34	1708.0			1144.90	1.43	7.08			14.00
0.50 0 0 3.09	0.00	*****				0.03168		1.13	7.00	5.78		14.00
902.27		6 80	1141.76					1 32	7 08			14 00
0.50 0 0.83	0.00	0.00	1141.70	1,00.0			0.02			5.78		14.00
0.50	1135.00	7 00	1142 00	1709 A								14.00
0.50 0	0.00	7.00	1142.00	1708.0	13.10	2.34	1145.02	0.00	7,08		8.00	14.00
Node 22 OTRANS STR	0.00000					0.01939	0.00					
0.50 0 903.10	1135.00	8.39	1143.39	1708.0	10.60	1.75	1145.14	1.29	6.82		9.00	15.00
	0.00 0.02953					0.01372	0.13			6.52		
0.50 0 912.47	1135.28	8,07	1143.35	1708.0	11,12	1.92	1145.27	1.39	6.82		9.00	15.00
	0.00 0.02953					0.01562	0.13			6.52		
0.50 0 921.10	1135.53	7.76	1143.29	1708.0	11.66	2.11	1145.40	1.51	6.82		9.00	15.00
0.50 0	0.00 0.02953						0.14					
0.50 0 928.80	1135.76	7.46	1143.22	1708.0	12.23	2.32	1145.54	1.64	6.82		9.00	15.00
0.50 0	0.00 0.02953						0.13					
0.50	1135.95		1143.11									15.00
0.50 0	0.00						0.02					13,00
0.50			1343 10									75 00
0.50 0 OHYDRAULIC	0.00	/ + Ja - J	T####	1,00.0	112.50	2.09	1143.09	1.00	6.0%		9.00	13.00
0.50	1135.97	£ 57	11 <i>40 80</i>	าวกจ ก	78 36	2 26	ijat co	9 5 75	c 55		0.00	15 00
£ 3 0	0.00		1140.47									12.00
0.50	0.02953		1140 00				0.16					
0.50 0	1136.13											15.00
0.50	0.02953											
0 962.71	1136.76	6.55	1143.31	1708.0	14.27	3.17	1146.47	2.15	6.82		9.00	15.00

									•			
0.50 0 0 8.12						0.02726	0.22			6.52		*
0.50 0 970.83 0.50 0	1137.00	6.82	1143.82									15.00
Node 23 TRANS STR						0.01910	0.00					
970.83	1137.00	8.08	1145.08	1708.0	10.54	1.73	1146.81	0.10	6.58		8.00	16.00
	0.00 0.02193					0.01364	0.23			6.85		
	1137.38	7.77	1145.15	1708.0	11.06	1.90	1147.05	0.10	6.58		8.00	16.00
0.50 0 0 17.95	0.00 0.02193					0.01555	0.28			6.85		
0.50 0 1005.97	1137.77	7.46	1145.23	1708.0	11.60	2.09	1147.32	0.11	6.58		8.00	16.00
0.50 0 0 10.47	0.00 0.02193					0.01718	0.18			6.85		
0.50 0 1016.44	1138.00	7.30	1145.30	1708.0	11.90	2.20	1147.50	0.12	6.58		8.00	16.00
0.50 0							0.00					
0.50 0 1016.44	1138.00	7,30	1145.30	1708.0	11.90	2.20	1147.50	0.00	6.58		8.00	16.00
0.50 0 Node 24												
OJUNCT STR 0,50	0.00000					0.01523	0.00					
0 1016.44 0.50 0	1138.00 0.00	7.94	1145.94	1653.0	10.42	1,69	1147.63	1.95	6.45		8.00	16.00
0 11.42 0.50	0.02593					0.01355	0.15			6.38		
	1138.30	7.63	1145.93	1653.0	10.93	1.86	1147.78	2.11	6.45		8.00	16.00
	0.02593					0.01545	0.17			6.38		
	1138.58	7.33	1145.91	1653.0	11.47	2.04	1147.95	2.29	6.45		8,00	16.00
	0.02593					0.01763	0.18			6.38		£.
	1138.84	7.04			12.03	2.25	1140.13	2.49	6.45		8.00	16.00
	0.02593			•		0.02012	0.19			6.38		
0 1058.36	1139.09	6.76	1145.85	1653.0	12.61	2.47	1148.32	2.71	6.45		8.00	16.00
	0.02593					0.02281	0.17			6.38		
	1139.28	6.52	1145.80	1653.0	13.16	2.69	1148.49	2.92	6.45		8.00	16.00
0.50 0 OHYDRAULIC												
0.50 0 1065.65	1139.28	6.38	1145.66	1653.0	13.50	2,83	1148.49	3.05	6.45		8.00	16.00
	0.00					0.02594	0.65			6.38		
0.50 0 1090.83	1139.93	6.38	1146.31	1653.0	13.50	2.83	1149.14	3.05	6.45		8.00	16.00
0.50 0 0 2.73						0.02548	0.07			6.38		
0.50 Node 25												
OTRANS STR 0.50						0.02502						
0.50 0	1140.00 0.00		1146.45									16.00
0.50	0.01148						0.03					
0.50 0		6.72	1146.74									16.00
0 5.47 0.50							0.11					
0.50 0			1147.08									16.00
0.50							0.22					
0.50 0		7.28	1147.51									16.00
/ 25.47							0.40					
0.50 0												16.00
	0.01148				F	0.01445	0.22			8.18		
	1140.69 0.00	7.68	1148.37	1653.0	10.86	1.83	1150.20	1.63	6.45		10.00	16.00

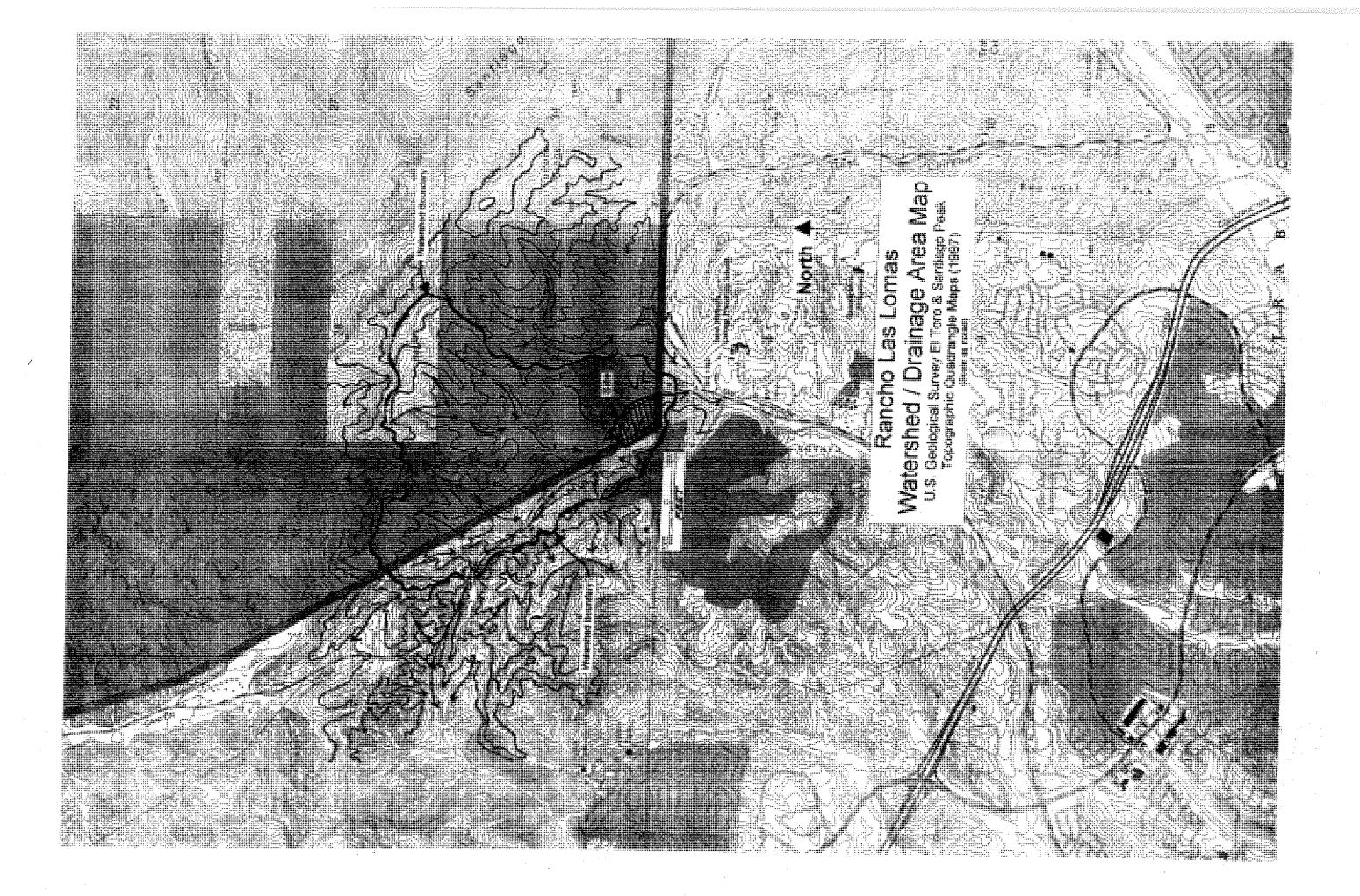
OHYDRAULIC .	JUMP											
0.50 0 1153.72	1140.69	5.35	1146.04	1653.0	16.55	4.26	1150.30	3.42	6.45		10.00	16.00
0.50 0 ( 0 3.65						0.04813	0.18			8.18		
0.50 01157.37	1140.73	5.20	1145.94	1653.0	17.07	4.53	1150.47	3.61	6.45		10.00	16.00
5.65						0.05391	0.30			8.18		
0.50 0 1163.02	1140.80	4.99	1145.79	1653.0	17.91	4.98	1150.77	3,93	6.45		10.00	16.00
0.50 0 0 0 5.82						0.06175	0.36			8.18		
0.50 0 1168.84	1140.86	4.79	1145.65	1653.0							10.00	16.00
0.50 0 0 0 5.91	0.00						0.42			8,18		10,00
0.50 0 1174.75		4.59	1145.52	1653.0							10.00	16.00
0.50 0 0 0 5.92	0.00	1,					0.48					10,00
0.50 0 1180.67		4.40	1145.40								10.00	16.00
0.50 0 ( Node 26			1110110	200011	20100	3.33	2202100	0.00	0.15		10.00	10,00
OTRANS STR	0.00000					0.05772	0.00				-	
0 1180.67 0.50 0 0		8.20	1149.20	1653.0	14.29	3.18	1152.38	2.63	8.20		11.00	10.00
0 2.24						0.02702	0.06			9.29		
0.50 0 1182.91 0.50 0 0		8.51	1149.55	1653.0	13.63	2.89	1152.44	2.43	8.20		11.00	10.00
0.50 0 10.56 0.50	0.01863					0.02381	0.25			9,29		
0 1193.48	1141.24	8.83	1150.06	1653.0	13.00	2.62	1152.69	2.25	8.20		11.00	10.00
0.50 0 0 0 37.66	0.01863					0.02098	0.79			9.29		
0.50 0 1231.14	1141.94	9.15	1151.09	1653.0	12.39	2.39	1153,48	2.08	8.20		11.00	10.00
0,50 0 0 0 3,21						0.01961	0.06			9.29		
.234.35		9.16	1151.16	1653.0	12.37	2,38	1153.54	2.07	8.20		11.00	10.00
0 0.00 C						0.01958	0.00			9.29		
0.50 0 1234.35		9.16	1151.16	1653.0	12.37	2.38	1153,54	0.00	8.20		11.00	10.00
0.50 0 0 Node 27												
OTRANS STR		0.16		7.650.0		0.01957						
0 1234.35 0.50 0 0	.00		1151.16	1653.0							12.00	10.00
0 22.33 0.50							0.41					
0 1256.68 0.50 0 0	.00		1151.79								12.00	10.00
0 46.62 0.50							0.76			10.30		
0 1303.30 0.50 0 0	.00		1152.74								12.00	10.00
0 8.04 0.50							0.12					
0 1311.34 0.50 0 0	1143.00 .00	9.88	1152.88	1653.0	11.19	1.95	1154.83	0.00	8.20		12.00	10.00
node 28 Otrans str	0.00000					0.00902	0.00					
0.50 0 1311.34	1143.00	11.38	1154.38	1653.0	6.13	0.58	1154.97	0.92	6.04		10.00	18.00
0.50 0 0 0 5.02	.00 0.07736					0.00323	0.02			4.22		
0.50 0 1316.36	1143.39	10.95	1154.34	1653.0	6.43	0.64	1154.98	1.00	6.04		10.00	18.00
0.50 0 0 0 4.78						0.00367	0.02			4.22		
0.50	1143.76	10.54	1154.30	1653.0	6.74	0.71	1155.00	1.08	6.04		10.00	18.00
1 0 0	.00 0.07736					0.00418	0.02			4.22		
0.50 0 1325.67	1144.11		1154.24	1653.0	7.07	0.78	1155.02	1.18	6.04		10.00	18.00
0.50 0 0						0.00476	0.02			4,22		
0.50 0 1329.97	1144.44	9.75	1154.19	1653.0	7.42	0.85	1155.04	1.28	6.04		10.00	18.00

0.50 0 0	.00											
0 4.04 (						0.00542	0.02			4.22		
0 1334.01 : 0.50 0 0		9.37	1154.12	1653.0	7.78	0.94	1155.06	1.38	6.04		10.00	18.00
0 3.79 ( 0.50							0.02			4.22		
337.80	1145.05 .00	9.01	1154.05	1653.0	8.16	1.03	1155.09	1.50	6.04		10.00	18.00
0 3.53 ( 0.50	0.07736					0.00704	0.02			4.22		
0 1341.33 3 0.50 0 0		8.65	1153.97	1653.0	8.56	1.14	1155.11	1.63	6.04		10.00	18.00
0 3.26						0.00803	0.03			4.22		
0 1344.59 3 0.50 0 0		8.31	1153.89	1653.0	8.97	1.25	1155.14	1.77	6.04		10.00	18.00
0 2.97 (						0.00916	0.03			4.22		
0 1347.56 3 0.50 0 0	1145.80	7.99	1153.79	1653.0	9.41	1.38	1155.16	1.92	6.04		10.00	18.00
0.50						0.01042	0.03			4.22		
0 1350.12		7.68	1153.68	1653.0	9.85	1.51	1155.19	2.08	6.04		10.00	18.00
0.50 0 0						0.01108	0.00			4,22		
0.50 0 1350.12		7.68	1153.68	1653.0	9.85	1.51	1155.19	0.00	6.04		10.00	18.00
0.50 0 0 Node 29 4'x4'	'RCB from of	ff-site				0.00905	0.00					
OJUNCT STR (		2 27	3354 37	1515 0				. 70			40.00	10.00
0 1350.12 1 0.50 0 0	.00	8.31	1154.37	1515.0								18.00
0 10.03 ( 0.50							0.08			5.35		
0 1360.15 1 0.50 0 0	.00	8.04	1154.35	1515.0							10.00	18.00
0 9.51 ( 0.50							0.08					
0 1369.66 1 0.50 0 0	.00	7.73	1154.31						5.71		10.00	18.00
8.79			4				0.09					
0 1378.45 0 0.50 0 0		7.42	1154.28	1515.0	9.40	1.37	1155.65	2.17	5.71		10.00	18.00
OHYDRAULIC JU 0.50												
0 1378.45 0 0,50 0 0	.00	4.27	1151.12						5.71		10.00	18.00
0 4.88 ( 0.50						0.06501	0.32			5.35		
0 1383.33 3 0.50 0 0.	1147.00 .00	4.17	1151.17	1515.0	18,10	5.09	1156.26	0:00	5.71		10.00	18.00
Node 30 OJUNCT STR (						0.06536	0.00					
0.50 0 1383.33		4.59	1151.59					0.00	6.08		10.00	15,50
0.50 0 0. 0 31.34 (	.00						1.97					
0.50 0 1414.67 1		4.59	1153.56								10.00	15.50
0.50 0 0. 0 63.62 0	.00						4.06		****			
0.50 0 1478.29		4.55	1157.54									15.50
0.50 0 0. 0 50.57 0	.00	*****	110,101				3.50	0.00		4.59		10.00
0.50 0 1528.86 1		л эп	1160 53					0.00				16 60
0.50 0 0. 0 22.78 0	.00	3.71	1100.33				1.81	0.00	0.00			13.50
0.50		4 10	1761 70					0.00				35 50
0 1551.64 1 0.50 0 0.		4.10	1101.10	1400.0	15.64	0.11	1101.30	V.VU	6.08		10.00	13.50
Node 31 OTRANS STR 0	0.00000					0.05682	0.00					
0.50 \\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	1157.60	7.62	1165.22	1460.0	13.86	2.99	1168.21	1.15	7.62		7.00	10.00
0 1.37 0						0.02706	0.04			9.35		
0.50 0 1553.01 1		7.91	1165.53	1460.0	13.22	2.72	1168.25	1.06	7.62		7.00	10.00
0.50 0 0. 0 5.35 0						0.02383	0.13			9.35		
0.50												

0 4558.37 1157.1 0.50 0 0.00	70 8.21	1165.91	1460.0	12,60	2.47	1168.38	0.98	7.62		7.00	10.00
0 12.29 0.0142 0.50	20				0.02099	0.26			9.35		
0 1570.65 1157.8 0.50 0 0.00	8.52	1166.39	1460.0	12.02	2.24	1168.63	0.91	7.62		7.00	10.00
0 26.44 0.0142	20				0.01849	0.49			9.35		
597.09 1158.2 0.50 0 0.00	8.84	1167.08	1460.0	11.46	2.04	1169.12	0.84	7.62		7.00	10.00
0 39.07 0.0142 0.50	20				0.01660	0.65			9,35		
0.30 0 1636.16 1158.6 0.50 0 0.00 Node 32	9.06	1167.86	1460.0	11.09	1.91	1169,77	0.00	7.62		7,00	10.00
OJUNCT STR 0.0000	0				0.01129	0.00					
0.50 0 1636.16 1158.8	10.33	1169.13	1405.0	6.43	0.64	1169.77	0.32	5.83		7.00	16.00
0.50 0 0.00 0 10.90 0.0339	)2				0.00408	0.04			5.31		
0.50 0 1647.06 1159.1	7 9.94	1169.11	1405.0	6.74	0.71	1169.82	0.34	5.83		7.00	16.00
0.50 0 0.00 0 10.46 0.0339	2				0.00464	0.05			5.31		
0.50 0 1657.52 1159.5	12 9.57	1169.09	1405.0	7,07	0.78	1169.87	0.37	5.83		7.00	16.00
0.50 0 0.00 0 10.02 0.0339	92				0.00528	0.05			5.31		
0.50 0 1667.53 1159.8	9,20	1169.06	1405.0	7.41	0.85	1169.92	0.41	5.83		7.00	16.00
0.50 0 0.00 0 4.01 0.0339	12				0.00577	0.02			5.31		
0.50 0 <b>16</b> 71.54 1160.0 0.50 0 0.00	9.05	1169.05	1405.0	7.56	0.89	1169.94	0.00	5.83		7.00	16.00
Node 33 OTRANS STR 0.0000	00				0.01913	0.00					
0.50 0 1671.54 1160.0	9.17	1169.17	1405.0	7.10	0.78	1169.95	1.19	5.63		8.00	17.00
0.50 0 0.00 0 7.69 0.0412	:7				0.00538	0.04			4.81		
0.50 Q= 1679.23 1160.3	2 9.82	1169.13	1405.0	7.44	0.86	1169.99	1.29	5.63		8.00	17.00
0 0.00 7.29 0.0412	:7				0.00613	0.04			4.81		
0.50 0 1686.53 1160.6	52 8.47	1169.09	1405.0	7.81	0.95	1170.04	1.41	5.63		8.00	17.00
0.50 0 0.00 0 6.89 0.0412	.7				0.00699	0.05			4.81		
0.50 0 1693.41 1160.9	0 8.14	1169.05	1405.0	8.19	1.04	1170.09	1.53	5.63		8.00	17.00
0.50 0 0.00 0 2.36 0.0412						0.02			4.81	- , - ,	
0.50 0 1695.77 1161.0		1169 03	1405 0	8 33				5 63		8 00	17 00
0.50 0 0.00 0 0.00 0.0412		1100103	210510			0.00		2,00			27100
0.50 0 1695.77 1161.0		1160 03	7405 0						4.01		17 00
0.50 0 0.00 Node 34	0.03	1109.03	1405.0	6,33	1.00	11/0,11	0.00	3.63			
OTRANS STR 0.0000	0				0.01699	0.00					
0.50 0 1695.77 1161.0	0 7.74	1168.74	1405.0	9.62	1.44	1170.18	3.61	6.04		8.00	15.00
0.50 0 0.00 0 9.44 0.0287	8				0.01215	0.11			5,83		
0.50 0 1705.21 1161.2	7 7.44	1168.71	1405.0	10.09	1.58	1170.29	3.92	6.04		8.00	15.00
0.50 0 0.00 0 7.63 0.0287	8				0.01370	0.10			5.83		
0.50 0 1712.84 1161.4	9 7.19	1168.68	1405.0	10.51	1.72	1170.40	4.20	6.04		8.00	15.00
0.50 0 0.00 OHYDRAULIC JUMP 0.50											
0 1712.84 1161.4 0.50 0 0.00		1166.50						6.04			15.00
0 0.02 0.0287						0.00					
.712.87 1161.4 0.50 0 0.00	9 5.01	1166.50	1405.0	16.02	3.99	1170.49	8.80	6.04		8.00	15.00
0 8.96 0.0287 0.50	8				0.05037	0.45			5.83		
0 .1721.83 1161.7 0.50 0 0.00 Node 35	5 4.81	1166.56	1405.0	16.80	4.38	1170.94	0.00	6.04	•	8.00	15.00

OTRANS STR	0.00000					0.00711	0.00					
0 1721.83 0.50 0	1161.75	4.31	1166.06	1405.0	17.94	5.00	1171.06	1.41	5.83		8.00	16.00
	0.06768					0.06311	3.03			4.29		
	1165.00	4.46	1169.46	1405.0	17.26	4.63	1174.09	0.00	5.83		8.00	16.00
	idge Outlet					0 10264	9.00					
0.50		4 45	17.00 4.0	* 105 0		0.10144						
0.50 0	1165.00 0.00 0.01988	4.40	1109.40	1405.0								16.00
0.50		4 40	3160.00	1405.0			0.37			4.36		
	0.00	4.49	1169.89	1405.0	1/.16	4.58	11/4.46	0.00	5.83		8.00	16.00
Node 37 Br						0.05907	0.00					
0.50 0 1789.97	1165.40	6.53	1171.93	1405.0	13.23	2.72	1174.65	0.28	6.53		7.00	13.00
0.50 0 0 7.80						0.02498	0.19			6.84		
0.50 0 1797.77	1165.58	6.79	1172.37	1405.0	12.61	2.47	1174.84	0.26	6.53		7.00	13.00
0.50 0 0 23.24						0,02311	0.54			6.84		
0.50 0 1821.01		6.84	1172.95	1405.0	12.52	2.44	1175.38	0.25	6.53		7.00	13.00
	0.00					0.02288	0.21			6.84		
0.50 0 1830.05		6.84	1173.15	1405.0	12.52	2.44	1175.59	0.25	6.53		7.00	13.00
0.50 0 OHYDRAULIC												
0.50 0 1830.05	1166.32	6.23	1172.55	1405.0	13.99	3.04	1175.59	0.31	6.53		7.00	13.00
0.50 0 0 4.45						0.03265	0.15			6.84		
0.50 0 1834.50		6.05	1172.47	1405.0	14.50	3.27	1175.73	0.33	6.53		7.00	13.00
0.50 0 0 6.41						0.03668	0,24			6.84		
	1166.57	5.81	1172.37	1405.0	15,21	3.59	1175.97	0.35	6.53		7.00	13.00
0.50 0 0 6.82						0.04186	0.29			6.84		
0.50 0 1847.73		5.58	1172.30	1405.0	15.95	3.95	1176.25	0.38	6.53		7.00	13.00
0.50 0 0 6.96	0.02288					0.04779	0.33			6.84		
0.50 0 1854.70	1166.88	5.36	1172.24	1405.0	16.73	4.35	1176.59	0.42	6.53		7.00	13.00
	0.02288					0.05458	0.38			6.84		
0.50 0 1861.66	1167.04	5.14	1172.18	1405.0	17.55	4.78	1176.97	0.45	6.53		7.00	13.00
0.50 0 0 6.89						0.06236	0.43			6.84		
0.50 0 1868.55	1167.20	4.94	1172.13	1405.0	18.40	5.26	1177.40	0.49	6.53		7.00	13.00
0.50 0 0 6.76						0.07128	0.48			6.84		
0.50 0 1875.30	1167.35	4.74	1172.09	1405.0	19.30	5.79	1177.88	0.54	6.53		7.00	13.00
	0.00					0.08151	0.54			6.84		
0.50 0 1881.90	1167.50	4.54	1172.05	1405.0	20.24	6.37	1178.42	0.58	6.53		7.00	13.00
0.50 0 0 6.42	0.02288					0.09326	0.60			6.84		
0.50	1167.65	4.36	1172.01	1405.0	21.23	7.00	1179.01	0.00	6.53		7.00	13.00
0.50 0 Node 38						~ ~~~						
OTRANS STR		2 40	55760				0.00					
0 7 0		7.88	11/5.53									11.00
1.75		0 0 0	N + MA A ··				0.07					
0.05 0	1167.70	t.25	1175.95									
0 · 7.78 0.05		5 44					0.29					•
0 1897.85	1167.92	8.64	11/6.55	1405.0	14.23	3.15	1179.70	0.47	7.88		7.00	11.00

0.05 0 0.00 0 23.20 0.02793 0.05					0.03308	0.77			9.42		
0 1921.05 1168.56	9.04	1177.61	1405.0	13.57	2.86	1180.47	0.43	7.88		7.00	11.00
0.05 0 0.00											
0 44.24 0.02793					0.03001	1.33			9.42		
0,05											
/ 1.965.29 1169.80	9.29	1179.09	1405.0	13.19	2.70	1181.80	0.40	7.88		7.00	11.00
0.00 ثُ											
0 0.00 0.02793					0.01447	0.00			9.42		
0.05											
0 1965.29 1169.80	9.29	1179.09	1405.0	13.19	2.70	1181.80	0.91	7.88		7.00	11.00
0.05 0 0.00											
Node 39 System Headwo	rks										



#### 100 YEAR FLOOD PLAIN CERTIFICATION

AUGUST 5, 2002

COUNTY OF DRANGE (PFRD) 300 N. FLOWER ST. SANTA ANA. CA. 92703

PROJECT: RANCHO LAS LOMAS

19191 LAWRENCE CANYON

SILVERADO, CA.

THIS LETTER IS TO CERTIFY THAT THE LOWEST FINISH FLOOR ELEVATION (F.F.E.) FOR ALL THE BUILDINGS LISTED BELOW BY BUILDING LETTER AND LOCATED ON THE ABOVE REFERENCED PROJECT ARE AT LEAST ONE FOOT OR GREATER ABOVE THE ADJACENT 100 YEAR FLOOD PLAIN LEVEL SHOWN ON HYDROLOGY REPORT DATED 5-27-02 PREPARED BY THIS FIRM AND ATTACHED HERETO AND BY REFERENCE MADE A PART HEREOF.

BUILD	 LOWEST FINISH FLOOR ELEVATION	100 YR. WATER SURFACE   FVFI
A AB	1132.3 1156.7	1123.4
AA	1162.5	1146.5 1149.2
C	1142.2 1143.4	1133.0 1134.9
E F	1136.5 1137.B	1133.0 1133.7
G	1145.5	1143.4
H	1156.9 1160.5	1146.5 1151.2
K L	1155.5 1168.3	1146.0 1165.2

T		
BUILDING LETTER	LOWEST FINISH FLOOR ELEVATION	100 YR. WATER SURFACE LEVEL
N	1176.0	1169.2
Р	1176.4	1171.9
Q	1176.6	1175.6
A	1176.5	1175.5
S	1179.1	1175.6
Т	1204.5	1175.6
U	1227.7	1175.6
٧	1229.1	1175.6
X	1154.9	1134.9
Y	1154.B	1134.9
Z	1163.0	1136.9

THE FOLLOWING LISTED BUILDINGS LOWEST FINISH FLOOR ELEVATIONS ARE NOT ONE FOOT ABOVE THE ABOVE REFERENCED 100 YR. FLOOD PLAIN LEVEL. THE EFFECT OF FLOODING HAS BEEN MITIGATED BY THE USE OF AN APPROXIMATELY TWO FOOT HIGH FLOOD CONTAINMENT WALL LOCATED ADJACENT TO SAID BUILDINGS. THE TOP OF WALL ELEVATION IS AT LEAST ONE FOOT OR GREATER ABOVE SAID 100 YR. FLOOD PLAIN LEVEL.

BUILDIN LETTER		TINISH 100 YR. EVATION SURFACE		TOP OF FLOOD CONTAINMENT WALL
AH	1138	1 113	8.B	1141.0
AG	1138		8.3	1140.4

PREPARED UNDER THE SUPERVISION OF:

COOK

<u>デージス</u> R.C.E. 31570 EXP. 12-31-04 PROFESSIONAL COOK STORY J. COOK J. COOK

TRITHIS ENGINEERING 2214 NEWPORT BLVD. (STE.A) COSTA MESA, CA. 92627 (949) 642-7442

GREGORY